

## Influence of the turbulence representation at the inlet on the downstream flow pattern in LES of backward-facing step

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**Abstract:** *The impact of the choice of inlet boundary condition treatment on the fluid flow is studied in this work. The correct representation of the turbulence at the inlet to the domain is essential for the accuracy of Large Eddy Simulation. The inappropriate specification of the inlet velocity has significant effect on the downstream flow pattern. The case of backward-facing step was used as a test case. Three different approaches of the inlet boundary conditions were studied: uniform velocity profile, mean velocity profile of the fully developed channel flow and velocity obtained from mapping velocity from plane positioned behind the inlet back to the inlet. The results of the simulations were compared with experimental results. It has shown, that using uniform velocity profile on inlet and even prescribing turbulent mean velocity profile without proper representation of turbulence fluctuations leads to unrealistic results.*

### 1 INTRODUCTION

In the simulation of turbulent flow, the most important factor seems to be proper choice of turbulence model that will provide good representation of the flow. Another issue of great importance is specification of boundary conditions, especially inlet boundary condition. The velocity and another inflow data linked with turbulence prescribed by boundary condition should be consistent with chosen turbulent model.

Description of mean velocity profile and other turbulence variables (turbulent kinetic energy, ...) obtained from analytical solution or from experiments can be regarded as sufficient for the RANS simulations. This approach was justified in [1]. It was shown that RANS model reach universal asymptotic behavior irrespective of the initial conditions. For Large Eddy Simulation, where the field on the inlet is turbulent, the situation is more problematic. Description of the flow is usually limited by knowledge of statistical quantities such as mean velocity profiles and mass fluxes. In LES, the data generated by inlet boundary condition should include an unsteady turbulent velocity signal representing turbulence at the inlet. Ideally, the simulation of upstream flow entering the computational domain will provide a good flow representation. However, unlimited extension in the upstream direction is not possible because of high computational cost. Therefore approximate inlet conditions must be specified.

A lot of methods were developed in the past. Kaltenbach et al. [2] used recycling method. Turbulent fluctuations are specified by running precursor simulation, whose only role is to provide main simulation with accurate boundary data. Another approach is to add synthetic turbulence at the inlet. Lund et al. [3] modified inlet velocity field by adding a random term to all velocity components. Klein et al. [4] proposed digital signal processing procedure to remedy lack of large- scale dominance in the inflow data generated by the random method.

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## 2 GOVERNING EQUATIONS

For the solution of the fluid flow in this article was chosen Large Eddy Simulation. The main idea of Large Eddy Simulation is to separate large scales (grid-scales) from small scales (subgrid-scales) to lower computational cost. The subgrid scales are modelled using subgrid model. The scale separation is done by applying filter operator on Navier-Stokes equation. If we apply the filter operator on Navier-Stokes equations we obtain filtered Navier-Stokes equations:

$$\frac{\partial \bar{u}_i}{\partial t} + \frac{\partial}{\partial x_j} (\bar{u}_i \bar{u}_j) = -\frac{1}{\rho} \frac{\partial \bar{p}}{\partial x_i} + \nu \frac{\partial^2 \bar{u}_i}{\partial x_k \partial x_k} - \frac{\partial \tau_{ij}}{\partial x_j}. \quad (1)$$

For evaluation of subgrid stress tensor  $\tau_{ij}$  is used Smagorinsky model:

$$\tau_{ij} - \frac{1}{3} \delta_{ij} \tau_{kk} = -2\nu_t \bar{S}_{ij}, \quad \nu_t = (C_S \Delta)^2 |\bar{S}| \quad (2)$$

$$\bar{S}_{ij} = \frac{1}{2} \left( \frac{\partial \bar{u}_i}{\partial x_j} + \frac{\partial \bar{u}_j}{\partial x_i} \right) \quad (3)$$

where  $|\bar{S}| = |2\bar{S}_{ij}\bar{S}_{ij}|^{1/2}$ .

## 3 DESCRIPTION OF THE TEST CASE

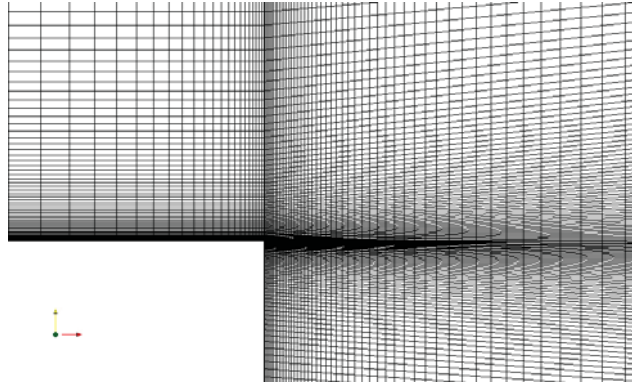
For testing of different approaches to the inlet boundary condition was chosen backward-facing step flow. This case of flow is good benchmark for validating various models because it contains massive separation and consequent re-attachment. Separation bubble on the wall opposite to the step could appear for some geometrical and flow parameters.

The geometry and flow properties was chosen according to the experimental study done by [6]. The Reynolds number of the inlet channel flow was 13 800, based on the bulk velocity of 10 m/s and the channel half-width of 20 mm. The expansion ratio was 5/3. The flow parameters of the inlet channel and backward facing step flow are in table 1.

**Table 1:** Flow parameters

Channel flow		Backward-facing step flow	
Channel half-width, $h$	20 mm	Step height, $H$	26.7 mm
Channel bulk velocity, $U_0$	10 m/s	Expansion ratio	5:3
$Re_h = \frac{U_0 h}{\nu}$	13 800	$Re_H = \frac{U_0 H}{\nu}$	18 400
$u_\tau$ , friction velocity	0.5 m/s	$\tau_f$ , large eddy time scale, $5H/U_0$	12.7 ms
Viscous length scale	31 $\mu\text{m}$		
Kolmogorov length scale, $\eta$	170 $\mu\text{m}$		

The computational mesh consists of 2.1 million hexahedral cells. The mesh is block-structured and becomes finer towards the wall in order to satisfy condition of  $y^+ \approx 1$ . The detail of the mesh near the trailing edge is in the Figure 1.



**Figure 1:** The detail of the mesh near the trailing edge.

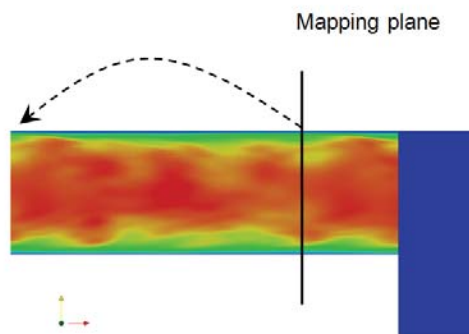
#### 4 INLET BOUNDARY CONDITION

For the generation of the velocity on the inlet to the domain were used three different approaches. Let them denote as Case A, B and C. All cases have bulk velocity of 10 m/s.

**Case A:** Uniform velocity profile is prescribed at the inlet to the computational domain. No velocity fluctuations are present.

**Case B:** Mean velocity profile of fully turbulent channel flow is prescribed on the inlet. No velocity fluctuations are present.

**Case C:** For the generation of the velocity on the inlet to the domain was used direct mapping approach [2]. The velocity on the inlet is obtained by direct mapping of the velocity from the plane with  $3h$  (60 mm) offset from the inlet plane. The schematic picture of the mapping is shown in the Figure 2 (the placement of the mapping plane in this figure is only schematic). For the flow initialization was used following procedure: First was done simulation of inlet channel only using periodic boundary condition. For faster transition to the fully developed turbulent flow was used forcing scheme based on Ornstein-Uhlenbeck process proposed by [7]. When the fully turbulent regime was reached then the results of this pre-simulation was mapped to the inlet channel of the backward-facing step geometry.

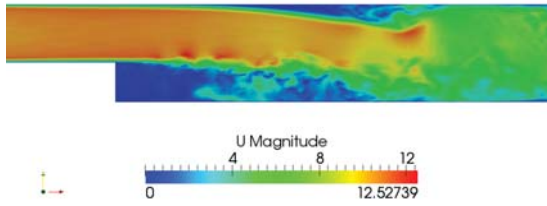


**Figure 2:** Scheme of inlet data mapping.

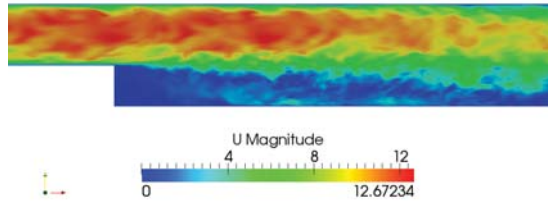
#### 5 RESULTS

In this section are described results obtained by various approaches to the inlet boundary condition. The simulations were started from zero velocity initial condition for cases A and B. The initial condition for case C could be seen in the Figure 2. The simulations ran for 0.5 s in order to allow development of turbulent structures in the domain. Then averaging was turned on and the simulations continued for another 1 s. This time was long enough to reach statistical steady state. The center of the coordinate system is positioned in the middle of the trailing edge.

In the figure 3 is instantaneous velocity magnitude for uniform velocity profile at the inlet (Case A). From this picture is evident that the velocity fluctuations are generated after the separation of the stream (behind the trailing edge). The lack of these fluctuations leads to the formation of the separation bubble on the top of the domain. The other consequence of the missing fluctuations is different shape of the recirculation region. For the mean velocity profile of fully turbulent channel flow described at the inlet (Case B) is situation similar. The instantaneous velocity magnitude for fully developed turbulent flow at the inlet (Case C) is in the picture 4. The flow pattern is much different from the previous one. There is no separation bubble on the top and the reattachment point is much further from the step.

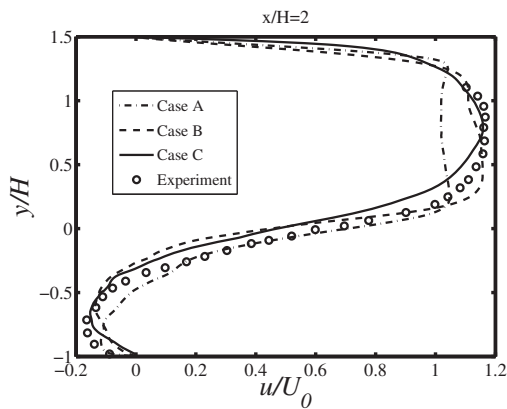


**Figure 3:** Instantaneous velocity for uniform inlet profile (Case A)

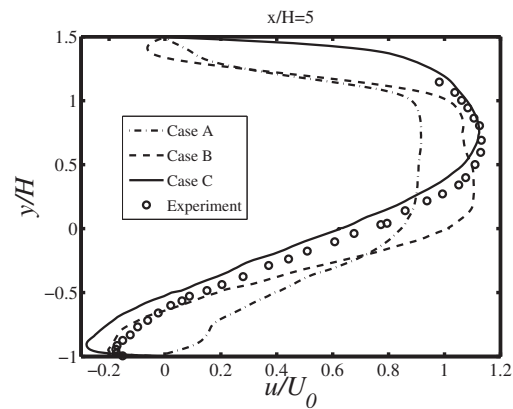


**Figure 4:** Instantaneous velocity for fully turbulent flow at inlet (Case C)

In the figure 5 are velocity profiles in short distance from the step. It could be noticed that the uniform inlet velocity gives nonrealistic results. From the flatness of the profile above the step could be stated that the length of the inlet channel is not long enough in order to develop turbulent velocity profile. Velocity profiles further from the step ( $x/H = 5$ ) are in the figure 6. Negative values of velocity at the top of the domain predicted in cases A and B indicates that separation bubble has been formed in this region. It is because of lack of wall-normal velocity fluctuation, which leads to absence of turbulent mixing mechanism and the main stream is bend down due the strong adverse pressure gradient. Case A also fails in prediction of re-attachment of the flow behind the step.



**Figure 5:** Velocity profile at position  $x/H=2$

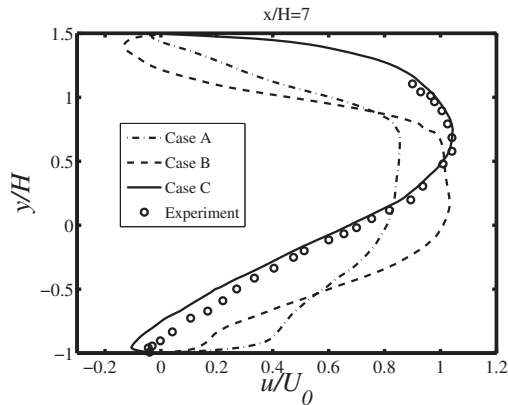


**Figure 6:** Velocity profile at position  $x/H=5$

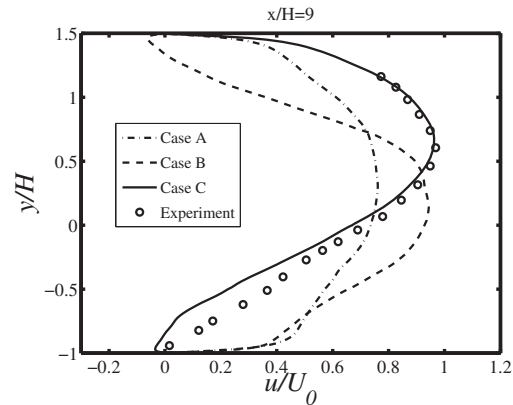
Figures 7 and 8 show situation far behind the step. Case B also fails in prediction of re-attachment. On the other side, case C predicts re-attachment point quite well. Re-attachment point predicted by case C is at position  $x/H = 9.2$  (experiment predicts this point at position  $x/H=8.4$ ).

## 6 CONCLUSIONS

The Large Eddy Simulation of backward-facing step was done. The simulations were done for three different representation of inlet boundary condition: uniform velocity profile, turbulent velocity profile and direct mapping of velocity from plane behind the inlet. Only the last case gives realistic results because is capable represent also turbulence velocity fluctuation. This has shown critical for the accuracy of the



**Figure 7:** Velocity profile at position  $x/H=7$



**Figure 8:** Velocity profile at position  $x/H=9$

simulation. The first two cases were not able to predict these fluctuations what resulted in the inclination of the incoming stream downwards and forming a separation bubble at the top of the domain. This is not in accordance with real experimental study. The inclination of the stream also affected the position of the re-attachment of the stream behind the step, the stream is re-attached too early.

The only proper way of representation of the inlet data presented in this work is running precursor simulation of the inlet channel using turbulence forcing and then mapping resulting fields to the main domain and direct mapping of velocity to the inlet. This is most complicated case but gives accurate results close to the experiment. The prediction of the re-attachment point could be improved by using more advanced subgrid model, for example some variant of localized Smagorinsky model [7].

## ACKNOWLEDGMENT

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