TISO ADJUSTABLE FILTER WITH CONTROLLABLE–GAIN VOLTAGE DIFFERENCING CURRENT CONVEYOR

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The main aim of this paper is to present solution of triple-input single-output (TISO) filter with independently adjustable pole frequency, quality factor, bandwidth and also gain. Filter is universal, operates in current mode and includes only one active element – the so-called Controlled-Gain Voltage Differenting Current Conveyor (CG-VDCC) with two controllable parameters: transconductance \(g_m\) and gain of output currents \(B_X\). Implementation of CG-VDCC element in 0.18 \(\mu\)m CMOS technology is also included and this model is used in proposed filter simulations.

Keywords: current mode, SITO filter, universal filter, CG-VDCC

1 INTRODUCTION

There have been many controllable active elements reported in recent works, brief summarization is given in [1]. Some active elements which have two externally controllable (by bias voltage or current) parameters have been already published. Typical examples of active elements with two-parameter control are modifications of the current differencing transconductance amplifier (CDTA) [2], where \(R_X\) and \(g_m\) control is implemented by DC bias currents [3, 4]. Several active elements, based on transconductance section (OTA) [1, 5] and current conveyor of second generation (CCII) [6, 7], have been also proposed. For example, current conveyor transconductance amplifier (CCTA) [8] also utilizes independent \(R_X\) and \(g_m\) control in some of its variants, for example [9]. Modification of CCTA in [10] employs current gain control, where current conveyor with adjustable gain from X to Z terminal was used. Controllable current gain in frame of current conveyor [11, 12] seems to be an interesting and valuable advantage [13–21].

Proposed novel active element provides useful controllable features. The so-called CG-VDCC consists of OTA and CCII elements (note that CCTA consists of the same active elements, but in reverse order). Our solution presented in this paper provides electronic control of \(g_m\) and of three current gains (each of them independently), therefore four parameters are controllable. As obvious from the presented transistor structure, \(R_X\) could also be controlled but it is not required in our case. This approach allows construction of very simple applications with minimum passive elements.

Active elements with more than one controllable parameter are very useful. They usually allow electronic control of more than one parameter of final filtering solution. In case of filter, it is pole frequency, quality factor, bandwidth and pass-band or stop-band gain [22]. Only one (more complex) active element is sufficient in many cases.

We provided a study of several universal filtering solutions and found following drawbacks concerning mainly lack of electronically controllable features of proposed applications:

• Not all parameters of the filter are adjustable independently and electronically [23],
• Too many active or passive elements are required [24, 25],
• Not all passive elements are grounded or outputs are taken from passive elements and therefore additional buffering is required [26, 27],
• Copies or inversions of input current are required (in case of presented filter, copies are required only for band-stop and all-pass filtering functions) [28],
• Absorption of parasitic input resistance is not possible [27, 29].

This paper is divided to two main parts. The first part deals with explanation of CG-VDCC behavior which is supported by simulations with CMOS model of proposed element. The second part discusses application of CG-VDCC in universal current-mode filter.

2 VOLTAGE DIFFERENCING CURRENT CONVEYOR

CG-VDCC element consists of transconductance section with electronically adjustable transconductance \(g_m\) and electronically controllable current conveyor of second generation with several outputs with electronically

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provides independent current gain of output current (by current $I_{\text{setB1-3}}$). One CA section has two outputs ($Z_P$ and $Z_N$, which means that first output is positive and the second one is negative), but only one of them is usually used in particular solution and therefore final transistor structure could be simplified according to particular requirements. If both outputs are present, their gain is the same, only the phase is inverted. If only one of this output is to be used and it is not decided if it is positive or negative, it is noted as $Z_B$ ($B$ is common sign for current gain).

Proposed CMOS model was simulated and analyzed with TSMC LO EPI 0.18 $\mu$m technology [31]. Some of important simulation results of CG-VDCC model are included in this paper. Figure 4 shows DC performance of OTA section for three values of control current $I_{\text{setgm}}$. Figure 5 shows AC performance of OTA section for the same three values of control current and Fig. 6 includes dependence of $g_m$ of OTA on control current.

Second group of graphs covers simulation results of MO-CCII and CA sections (connected together as a second part of a structure depicted in block diagram). Figures 7 and 8 contains DC and AC responses for three particular values of gain control current and Fig. 9 includes dependence of control gain on control current.

DC parameters of CG-VDCC element are as follows: $R_{V+} = R_{V-} > 1 \Omega$, $R_Z = 52 \, k\Omega$, $R_X = 450 \, \Omega$ ($I_{\text{setRX}} = 150 \, \mu A$), $R_{ZP} = R_{ZN} = 58 \, k\Omega$ (when $B = 1$). Transconductance can be controlled from 255 $\mu$S to 1919 $\mu$S (by $I_{\text{setgm}} = 10 \, \mu A$ to 150 $\mu A$) and current gain can be controlled from 0.36 to 3.76 (by $I_{\text{setB1-3}}$ from 100 $\mu A$ to 20 $\mu A$).
3 EXAMPLE OF FILTERING SOLUTION WITH CG–VDCC

Proposed active element is very suitable for design of electronically controllable filters. This section presents an example of current-mode TISO universal controllable filter with only one CG-VDCC. Its structure is shown in Fig. 10.

Ideal transfer functions (low pass = LP, inverting band pass = iBP, high pass = HP, band stop = BS, all pass = AP).
Fig. 6. Dependence of $g_m$ of OTA on control current, $V_{DD} = -V_{SS} = 1 \, V$, $V- = X, Z, Z_{PB1-3} - GND$

Fig. 7. MO-CCII and CA section DC performance for selected values of control current, $V_{DD} = -V_{SS} = 1 \, V$, $V+ = V-, Z - GND$

Fig. 8. MO-CCII and CA section AC performance for selected values of control current, $V_{DD} = -V_{SS} = 1 \, V$, $V+ = V-, Z - GND$

Fig. 9. Dependence of current gain of MO-CCII and CA section on control current, $V_{DD} = -V_{SS} = 1 \, V$, $V+ = V-, Z - GND$

Fig. 10. Structure of TISO universal controllable filter

AP) of this filter are

$$K_{LP}(s) = \frac{I_{OUT}}{I_{IN1}} = \frac{B_1 G_1 g_m}{D(s)},$$

if $I_{IN1} = -I_{IN}$ and $I_{IN2} = I_{IN3} = 0$;

$$K_{IBP}(s) = \frac{I_{OUT}}{I_{IN2}} = \frac{-B_1 s C_1 G_1}{D(s)},$$

if $I_{IN2} = I_{IN}$ and $I_{IN1} = I_{IN3} = 0$;

$$K_{HP}(s) = \frac{I_{OUT}}{I_{IN3}} = \frac{s^2 C_1 C_2 B_1}{D(s)},$$

if $I_{IN3} = -I_{IN}$ and $I_{IN1} = I_{IN2} = 0$;

$$K_{BS}(s) = \frac{I_{OUT}}{I_{IN1} + I_{IN3}} = \frac{s^2 C_1 C_2 B_1 + B_1 G_1 g_m}{D(s)},$$

if $I_{IN1} = -I_{IN}$ and $I_{IN3} = I_{IN}$ and $I_{IN2} = 0$;

$$K_{AP} = \frac{I_{OUT}}{I_{IN1} + I_{IN2} + I_{IN3}} = \frac{s^3 C_1 C_2 B_1 - B_1 s C_1 G_1 + B_1 G_1 g_m}{D(s)},$$

when $B_1 = 1$, $B_2 = -1$, $B_3 = -1$. 

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Phase shift (deg)

Magnitude response of iBP for three different values of gain $g$

Fig. 12. Magnitude response and phase shift of AP filter when $B_1 = 1$, $B_2 = -1$, $B_3 = -1$

Gain control: magnitude response of iBP for three different values of gain $B_1$ when $B_2 = -1$, $B_3 = -1$

Quality factor control: magnitude response of iBP for three different values of gain $B_3$ when $B_1 = 1$, $B_2 = -1$

Center frequency control with constant bandwidth: magnitude response of iBP for three values of gain $B_2$

Center frequency control with constant quality factor: magnitude response of iBP for three values of gain $B_3$

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$f_C = 1$ MHz is starting pole frequency for $g_m = 690 \mu S$ ($I_{set, gm} = 33 \mu A$) and $G_1 = 1$ mS, $Q = 0.707$ (Butterworth approximation) for $B_3 = -1$, $C_1 = 155$ pF, $C_2 = 78$ pF. Some of simulation results are summarized in Figs. 11–16. The first figure, Fig. 11 shows overall filter response for starting parameters as mentioned before in case of LP, iBP, HP and BS function, Fig. 12 shows characteristics of AP filter in the same conditions. Figs. 13–16 present possibilities of control in case of iBP response. Figure 13 includes gain control, Fig. 14 shows control of center frequency with constant bandwidth, Fig. 15 control of quality factor with constant center frequency and finally, Fig. 16, tuning of center frequency with constant value of quality factor.

4 CONCLUSION

Presented filtering solution has many advantages thank to electronic control of four parameters: $g_m$ and of three independent current gains, therefore four parameters are controllable mutually independently as described briefly in Section 3. Filter consists of one active element and three passive elements, but $G_1$ could be omitted if control of pole frequency independently on quality factor and some of filtering functions is not required. From Figs. 11–16 it is obvious that there are some parasitic influences, for example in case of HP response (Fig. 11), pass-band gain is not unity (0 dB). In this particular case it is caused by $R_X$ of $X$ terminal that acts as current divider with $G_1$. Note that this is not a problem, because gain could be fine-tuned by $B_1$ without affecting any other parameter of the filter. The same method could be used to fine-tune gain in case of quality factor adjustment (Fig. 15). All control processes were presented only on band pass response but tuning is also possible in case of other filtering functions. The main advantages of final filtering solution are

- all parameters of the filter are adjustable independently and electronically,
- not many active and passive elements are required,
- all passive elements are grounded and no output is taken from passive element and therefore additional buffering is not required,
- absorption of parasitic input resistance ($R_X$) is possible, its expected values have been taken into calculations.

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