

# Co-channel and Adjacent Channel Interference Measurement of UMTS and GSM/EDGE Systems in 900 MHz Radio Band

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**Abstract.** This paper is concerned with inter-system and intra-system interference measurements of 2.5G and 3G mobile communication systems. The both systems UMTS and GSM/EDGE are assumed to operate in a common radio band of 900 MHz. The main system parameters are briefly introduced as well as the measurement scenario. Several simulations and key measurements were performed. Important results are described and commented along with a graphical representation, namely bit error ratio (BER) dependence on carrier to noise ratio (CNR) in the presence of additive white Gaussian noise (AWGN), the measurement of adjacent channel interference ratio of each system, the coexistence of both systems in same band and the impact of a carrier offset on BER.

## Keywords

UMTS, GSM/EDGE, interference, measurement, co-channel, adjacent channel, BER, carrier offset.

## 1. Introduction

The radio spectrum becomes occupied very densely nowadays. Thus, radio planning and management is a vital question of present studies and papers.

The performance of any radio system is interference dependent. The aim of this work is the coexistence investigation of the mobile wireless systems UMTS and GSM/EDGE. The main aspect observed is co-channel and adjacent channel interference, while both the systems operate in the common radio band of 900 MHz.

Frequency planning is assumed, in which a UMTS carrier is sandwiched between existing GSM carriers with sufficient guard bands between the carriers (see Fig. 1). The size of guard bands is the subject of examination, because there could be possible capacity loss due to the adjacent channel interference.

Standard rules for the guard bands are based on nominal assumptions about the adjacent channel selectivity (ACS) of the receivers and the adjacent channel leakage

(ACLR) of the transmitters. It has been shown that interference from GSM uplink onto the UMTS uplink is the dominant cause of capacity loss. The use of adaptive filters on UMTS Node B transceivers, with the ability to selectively reject interfering GSM uplink signals, can essentially reduce the size of guard bands [4].

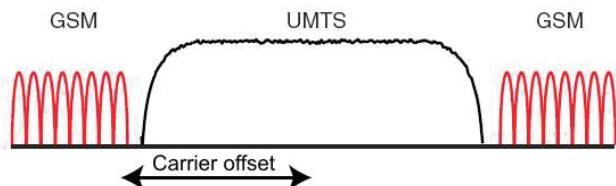


Fig. 1. Frequency plan – “sandwich” type of UMTS band between GSM bands.

## 2. Measurement Scenario

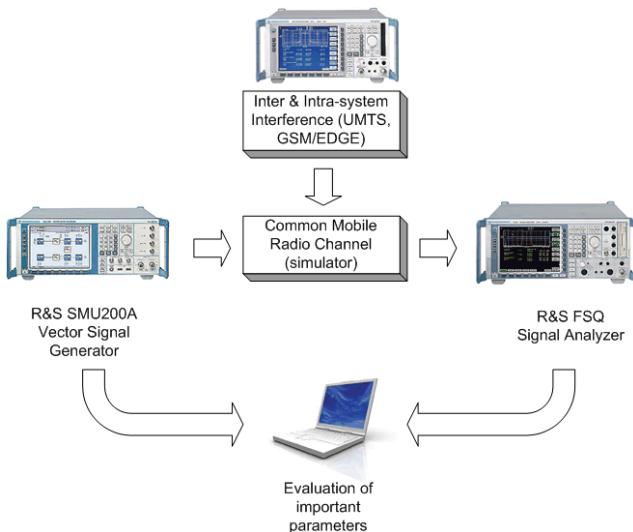
It is very important to distinguish a measurement in a laboratory and a real-time measurement on an operating base station. There are clearly defined conditions in a laboratory in terms of fixed parameters. Moreover, the radio channel is simulated in a deterministic way. This method is suitable for cases that need reproducible testing, while the measurement in the real network reveals the real system behavior and operation. However, this method needs portable equipment and a direct access to the network [1].

In these terms experimental measurement in the lab conditions was chosen. The direct access to the real network is not possible due to the non-existence of pure UMTS-FDD network in the Czech Republic.

A signal generator R&S corresponds to a useful transmitting device (UE) in the uplink. The source of interfering signal is another signal generator R&S. The channel conditions are directly set at the signal generators. Both the useful and interfering signals are then coupled together on the common cable. This mixed signal is led to the signal analyzer R&S, which corresponds to the receiver (BTS, Node B). Transmitted and received signals are after that analysed and the qualitative parameters are evaluated. The whole process can be seen in Fig. 2.

## 2.1 The System Overviews

The UMTS system is based on direct sequence code division multiple access (DS-CDMA). The spreading sequence has a constant chip rate equal to 3.84 Mchip/s. The user data signal has a variable bit rate from 15 kbit/s to 960 kbit/s in the uplink direction (from a mobile station to a base station). The rate between the chip rate and bit rate is called spreading factor (SF). The values of SF are from 4 to 256 and are always a power of 2.



**Fig. 2.** Measurement scenario.

The basic operations, which are performed with the signal, are spreading and scrambling. The signal is first spread by the OVSF code (Walsh codes are used). This leads to an extension of the signal band to approximately 5 MHz. After that, the wideband signal is scrambled by scrambling code (S(2) or Gold codes are used). This operation does not cause additional extension of the bandwidth.

In UMTS uplink, the channels are I-Q/code multiplexed. This is also called dual-channel QPSK modulation. The carrier raster is 200 kHz. More information can be found, for example, in [2] and [5].

The GSM/EDGE system (frequently referred to as EGPRS – Enhanced General Packet Radio Service) is a direct evolution of GPRS. The same concept and architecture are used – 200 kHz channel bandwidth, the combination of FDMA/TDMA multiple access, 8 timeslots, etc [6]. The main changes are in the radio interface in comparison with GPRS.

A new modulation and coding scheme (MCS) enables optimization of transfer rate with respect to radio environment conditions. Data bit rates (on the RLC/MAC layer) start at 8.8 kbit/s per slot (MCS-1) and end at 59.2 kbit/s per slot (MCS-9) [6]. The first four schemes utilize the GMSK modulation, the remaining five schemes utilize the 8-PSK modulation.

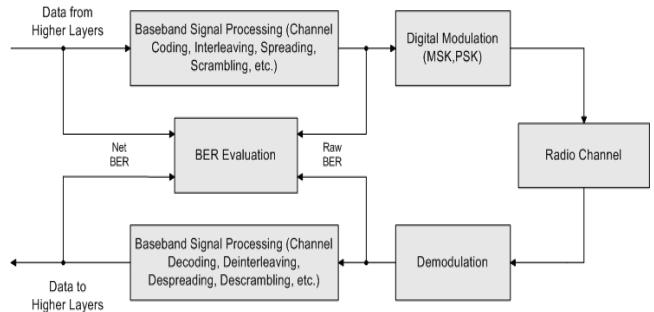
## 2.2 Simulation Setup

Both physical layer models of the system have been designed and implemented in Matlab according to the 3GPP standards and recommendation [5] – [11].

In the UMTS mode, UE maintains data connection with a variable bit rate, which is set by the spreading factor. It starts from SF = 256 and after 1000 frames it is switched in a descending order until SF = 4 is reached.

In the GSM/EDGE mode, UE also maintains data connection with a variable bit rate, which is here set by modulation and by the coding scheme. It starts from MCS-1 and after 1000 frames it is switched in an ascending order until MCS-9 is reached. No retransmissions are considered. Forward error correction is assumed only.

The scheme of BER computation is depicted in Fig. 3. The useful signal net BER is evaluated at the top of the physical layer. In the case of GSM/EDGE signal it is the BER of RLC/MAC blocks. In the case of UMTS signal it is the BER of transport data blocks (TB). The useful signal raw BER is evaluated right after a demodulation before the channel decoding. The simulations have been done for AWGN channel so far [13], [14]. They are utilized in section 3.1 for comparison with measured values. The simulations for the adjacent channel interference investigation are under testing at present.



**Fig. 3.** Block scheme of Matlab Simulation.

## 2.3 Measurement Setup

In order to create reproducible tests it is necessary to set up the testing scenarios. The UMTS system provides several variants of signals, which are dependent on spreading factor, amount of timeslots and codes assigned etc. Therefore the reference channels were defined. Primarily, the UE has to support the channel of 12.2 kbit/s rate (usually for voice communication). Next channels (especially for data transmission) are of 64, 144 and 384 kbit/s rates. These channels are briefly described in Tab. 1. Each channel has a constant chip rate 3.84 Mchip/s and a constant bandwidth 5 MHz.

Also the GSM system provides plenty of channels with various bit rates, which are defined by modulation and coding scheme (MCS) [6]. However, for the adjacent channel interference investigation only the symbol rate

270.833 ks/s, modulation GMSK or 8-PSK and the channel bandwidth 200 kHz is important.

Parameter	Channel 1	Channel 2	Channel 3	Channel 4
User bit rate (kbit/s)	12.2	64	144	384
DPDCH (kbit/s)	60	240	480	960
DPCCH (kbit/s)	15	15	15	15
Spreading factor	64/256	16/256	8/256	4/256
DPDCH/DPCCH				

Tab. 1. UMTS reference channels (uplink).

One of the many important factors is the signal bandwidth limitation to prevent interference to adjacent bands. The UMTS signal bandwidth is chip rate dependent. So the bandwidth needed is approx. 3.84 MHz. The used raised-root cosine (RRC) filter, which performs pulse shaping and prevents from inter symbol interference ISI, broadens this bandwidth about 22 % (roll-off factor 0.22) to approx. 4.6 MHz. The standardized bandwidth is 5 MHz [1].

The GSM/EDGE signal bandwidth comes from symbol rate and used Gaussian filter ( $bt = 0.3$ ). It occupies approx. 400 kHz. Standardized bandwidth is 200 kHz. However, due to filtration the suppression on the adjacent carrier is approx. 60 dB [3].

In real systems, there are several effects, which forbid the creation of ideal signal with defined spectrum. These are foremost nonlinear amplifiers, which transmit the part of energy to the adjacent bands. It is necessary to verify these parts of power in adjacent bands. For these purposes, adjacent channel leakage power ratio (ACLR) of the two closest channels (adjacent and alternate) is defined. In the case of UMTS, the two measured channels are off 5 and 10 MHz. In the case of GSM/EDGE, these channels are off 200 and 400 kHz. The power suppression of UE in the uplink has to be greater than 33 dBc for adjacent channel and 43 dBc for alternate channel [1], [3].

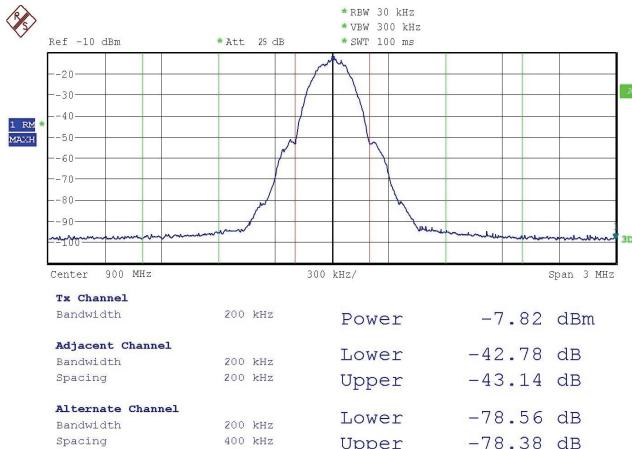


Fig. 4. GSM/EDGE ACLR measurement.

The measured spectra of both the signals in the 900 MHz band can be seen in Fig. 4 and 5. The exact measured values are summarized in Tab. 2 and 3. As can be seen, both system signals spectra satisfied the requirements.

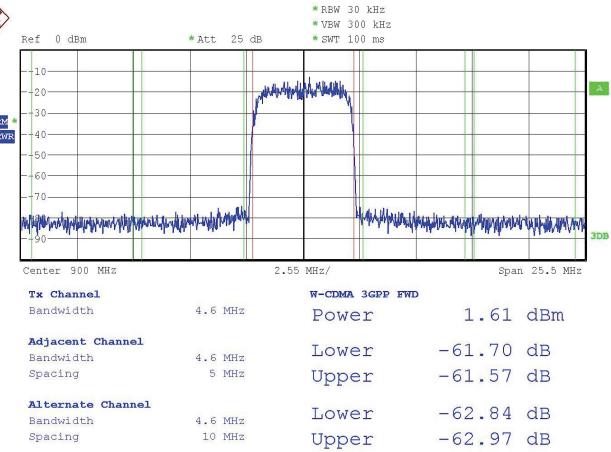


Fig. 5. UMTS ACLR measurement.

Adjacent channel distance	Measured ACLR (absolute value)	ACLR limit
+200 kHz	35,32 dB	33 dBc
- 200 kHz	34,96 dB	33 dBc
+ 400 kHz	70,56 dB	43 dBc
- 400 kHz	70,74 dB	43 dBc

Tab. 2. Confrontation of measured and required ACLR values (GSM/EDGE).

Adjacent channel distance	Measured ACLR (absolute value)	ACLR limit
+ 5 MHz	61,57 dB	33 dBc
- 5 MHz	61,70 dB	33 dBc
+ 10 MHz	62,97 dB	43 dBc
- 10 MHz	62,84 dB	43 dBc

Tab. 3. Confrontation of measured and required ACLR values (UMTS).

The next required feature is the receiver selectivity (ACS – Adjacent Channel Selectivity) and its rejection of adjacent bands. In other words, it is necessary to find out how the quality of useful signal is affected by presence of neighboring interferer. Thus, the ACS is a measure of a receiver capability to receive a useful signal on a certain carrier frequency in presence of other signals in adjacent channels. The nominal allowable value is defined as 33 dB providing that the maximum power of the adjacent signal will not exceed -25 dBm. The last but not least important thing is the intermodulation products rejection. More details can be found in [3]. The adjacent channel selectivity measurement will be implicated in the adjacent channel interference system performance (section 3.2 and next).

### 3. Results

The following sections provide both the measured and simulated results. Section 3.1 verifies the minimum required values of CNR or  $E_b/N_0$  for reaching the nominal raw BER  $10^{-3}$ . Sections 3.2 and 3.3 provide performance of both the UMTS and GSM/EDGE systems in presence of adjacent interferers. Finally, section 3.4 provides coexistence measurements under operation in common radio band for frequency planning of the sandwich type (see section 1).

#### 3.1 Single System Operation in Presence of AWGN

The measurement and simulation for GSM/EDGE system was split into two parts – for the GMSK modulation and coding schemes MCS-1 to MCS-4 and for the 8-PSK modulation and coding schemes MCS-5 to MCS-9. The measurement equipment supports only raw BER evaluation, so the curves of measured dependences are always of raw BER while simulated are of net BER (after channel decoding and other physical layer baseband operations). In Fig. 6, there are curves for coding schemes MCS-1 and MCS-4, which provide the most and the least error protection for the GMSK modulation, followed by the measured GSM/EDGE modulated signal (GMSK) and a theoretical curve for the GMSK modulation for comparison. The CNR is about 8.5 dB for reaching nominal raw BER  $10^{-3}$  and for measured and theoretical signal while the required value given by standards is 9 dB. A simulated curve for the MCS-1 shows the best performance because of the highest protection while the MCS-4 it shows the worst performance because of a weak protection, but from CNR = 11 dB shows almost the same progression as the measured curve. The coding gain of MCS-1 is about 3 dB in comparison with the measured signal.

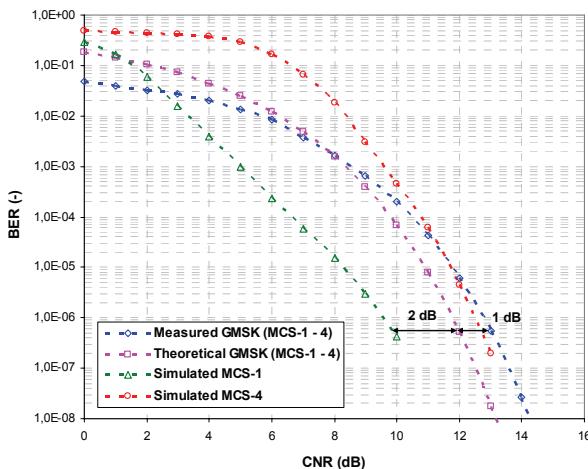


Fig. 6. Comparison of measured and simulated values of BER dependence on CNR, GMSK modulation, AWGN.

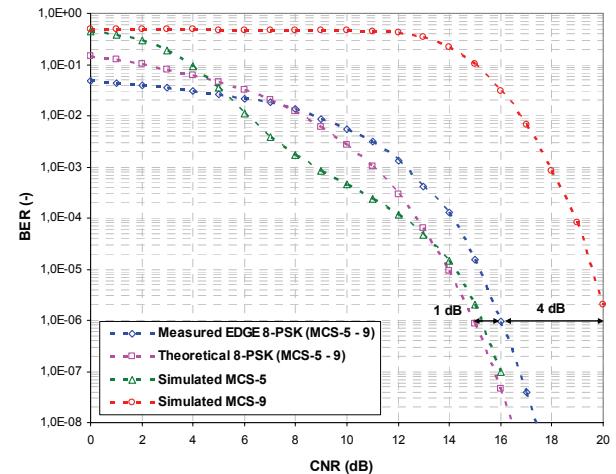


Fig. 7. Comparison of measured and simulated values of BER dependence on CNR, 8-PSK modulation, AWGN.

In Fig. 7, there are curves for the coding schemes MCS-5 and MCS-9, which provide also the most and the least error protection but now for the 8-PSK modulation, followed by the measured GSM/EDGE modulated signal (8-PSK) and the theoretical curve for the 8-PSK modulation. The simulated curve for the MCS-5 shows again the best performance because of the highest protection, but from CNR = 14 dB it shows almost the same progression as the measured curve (with 1 dB coding gain for the MCS-5). The MCS-9 shows the worst performance because of almost no protection (high order of puncturing, 2/3 of data part is leaved). The coding scheme MCS-9 is about 4 dB behind the rest.

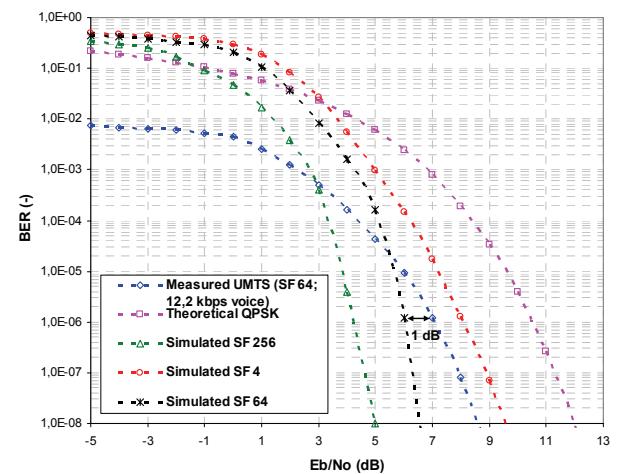


Fig. 8. Comparison of measured and simulated values of BER dependence on  $E_b/N_0$ , QPSK modulation, AWGN.

Measurement and simulation for the UMTS system also brings no greater differences. The measured reference channel was 12.2 kbit/s (see Tab. 1). For comparison, the channel with the same SF = 64 was simulated along with the channels with the lowest and the highest SF = 4 and 256. Simulated curves firstly show higher BER because of the protection, but from a certain point there is a significant

gain. The required value of  $E_b/N_0$  given by standards for 12.2 kbit/s reference channel is 5 dB for reaching nominal raw BER  $10^{-3}$ . Both compared signals of SF = 64 meet this requirement.

### 3.2 GSM/EDGE Intra-system Interference

This section provides GSM/EDGE system performance in presence of co-channel and adjacent channel interferer. This interfering signal comes from the same system. Hence, it is called the GSM/EDGE intra-system interference.

The measurements were done for the carrier offset of 200, 400 and 600 kHz. The other higher offsets are not considered, since the dynamic range of GSM receiver is about 80 dB. The useful signal was disturbed by strong interferer on the common channel. The receiver has performed raw BER evaluation of the useful signal in dependence of useful-to-adjacent channel interference power ratio (C/Ia). The required values of a minimum C/Ia ratio for reaching nominal raw BER  $10^{-3}$  are introduced in Tab. 4.

Carrier offset (kHz)	Required values of C/Ia (dB)	Measured values of C/Ia (dB)
0	9	8
200	- 9	- 16
400	- 41	- 40
600	- 49	- 55

Tab. 4. C/Ia requirements and measured values for GSM/EDGE system.

As it can be seen, all the requirements were satisfied, somewhere even with a reserve, except of 400 kHz carrier offset. In this case, the measurement is 1 dB above tolerance, but this can be assigned to the inaccuracy of the measurement.

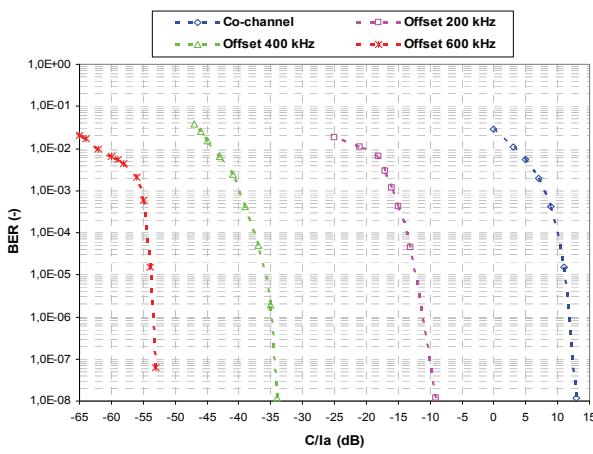


Fig. 9. GSM/EDGE BER performance in adjacent channel intra-system interference conditions.

Thus, good filtering of received signal is a basic tool to challenge the adjacent channel interference. The better performance is possible only with a fast power control. The

co-channel interference can be minimized by good frequency planning. The most potential danger is the adjacent channel interference right in the next channel (200 kHz offset) when the UE is close to the other base station and other UE operating in adjacent channel (risk of blocking).

### 3.3 UMTS Intra-system Interference

This section provides the same content as previous, but results here are concerned with the UMTS performance in presence of adjacent channel interferer.

The measurements were done for the carrier offset of 5 and 10 MHz, other higher offsets are meaningless from identical reason. The results of raw BER evaluation of a received useful signal in dependence on the adjacent channel interference power ratio (C/Ia) are shown in Tab. 5 and graphically in Fig. 10.

Carrier offset (MHz)	ACIR values (dB) (for comparison)	Measured values of C/Ia (dB)
0	---	6
5	- 33	- 39
10	- 43	- 52

Tab. 5. C/Ia requirements and measured values for UMTS system.

Measured values have also satisfied the requirements in terms of the ACIR (Adjacent Channel Interference Ratio). The co-channel interference can be minimized only by the fast power control. The potential danger is the same as in the previous section - the adjacent channel interference (5 MHz offset) when the UE is close to the other base station and other UE. There is a need to assure at least 35 dB isolation of interfering UEs, which corresponds to about 20 m of a distance separation for the free space path loss formula. For the Okumura-Hata model and urban environment [13] it is about 3 m.

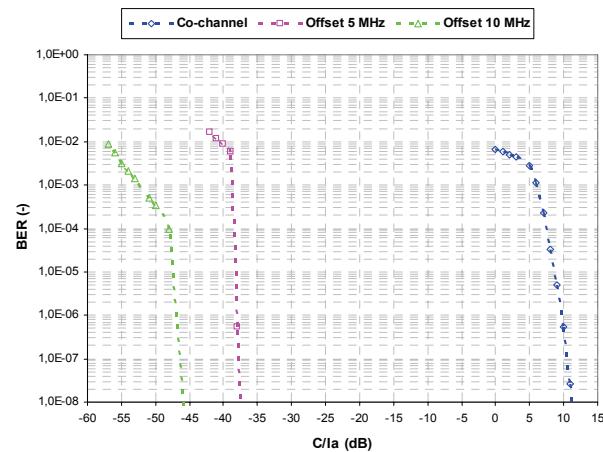


Fig. 10. UMTS BER performance in adjacent channel intra-system interference conditions.

These results are valid also for GSM/EDGE. It is assumed that both systems operate in 900 MHz radio band,

height of base stations is approx. 25 m, height of UEs is approx 1.5 m.

### 3.4 Coexistence Investigation and Inter-system Interference

The benefits of UMTS900 are all a result of the lower carrier frequency. UMTS at 900 MHz will propagate further than its equivalent at 2100 MHz. Better propagation also means the interference will propagate better. The increase of interference due to better propagation conditions must be considered [4].

The measurement scenario was the following: both the useful GSM/EDGE and UMTS interfering signals were transmitted on the common channel. The power of signals with 1 dB step was set on the output of both transmitters. The receiver was matched to the useful GSM/EDGE signal and has performed the evaluation of BER in dependence on a power setting. The same measurement was done for the UMTS signal as useful and GSM/EDGE as interfering. The results achieved are presented in Fig. 11 and 12.

Carrier offset (MHz)	UMTS useful	GSM useful
Up to 2	Not sufficient	Not sufficient
2.2	Not sufficient	Not sufficient
2.4	Borderline	Not sufficient
2.6	Enough	Borderline

Tab. 6. Summary of an interference impact.

As it can be seen from both figures, there is a significant reduction of performance or in other words there is an increase of interference level if the carrier separation is up to 2.2 MHz.

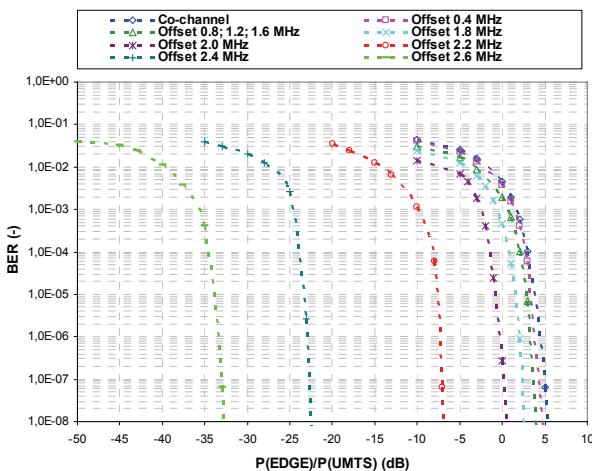


Fig. 11. GSM/EDGE performance in presence of interfering UMTS signal, BER dependence on interfering signal power and carrier spacing.

In case of GSM/EDGE useful signal and 2.4 MHz carrier separation, there is a reserve of 25 dB to meet the nominal

raw BER  $10^{-3}$ . This value is not so high and can cause quality degradation. For 2.6 MHz carrier separation, there is a reserve of 35 dB. This value is sufficient for good quality communication (in terms of distance separation).

In case of UMTS useful signal and 2.4 MHz carrier separation, there is a reserve of 37 dB. This value is sufficient as was mentioned above. For 2.6 MHz, there is even 48 dB reserve. This value will neither limit the quality nor capacity of the system. The interference level will not be increased. As can be seen, the UMTS signal is more resistant than the GSM/EDGE signal.

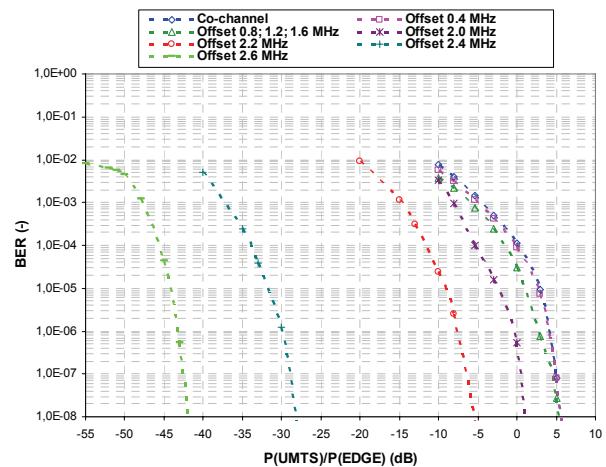


Fig. 12. UMTS performance in presence of interfering GSM/EDGE signal, BER dependence on interfering signal power and carrier spacing.

For uncoordinated deployment of the UMTS system between the existing GSM/EDGE system in 900 MHz band, there should be minimum carrier spacing of 2.6 MHz. 2.4 MHz is on the borderline. Less separation causes the significant increase of interference. So there is no need to utilize the whole 5 MHz bandwidth for the UMTS signal, hence make the frequency planning more efficient.

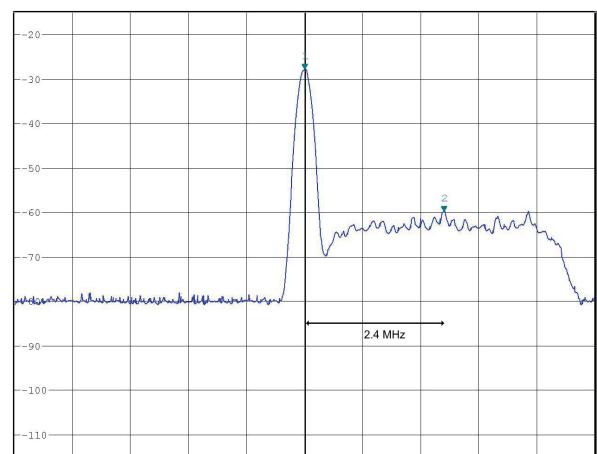


Fig. 13. Carrier separation of 2.4 MHz, the minimum borderline (common spectrum of GSM/EDGE and UMTS signal).

## 4. Conclusions

This paper provides some measurement and simulation results for the GSM/EDGE and the UMTS signal in presence of the adjacent channel interference.

Basic parameters of both systems and requirements for inter-working were presented as well as the simulation and measurement scenario.

The minimum CNR ( $E_b/N_0$ ) values to meet the nominal BER  $10^{-3}$  were verified on the AWGN channel. The fulfillment of the ACS and the ACLR was also verified in a particular measurement.

The curves of intra-system interference from sections 3.2 and 3.3 show potential risks especially in GSM/EDGE system for the 200 kHz adjacent channel interference. The isolation here is very poor, so the good frequency planning and power control is a crucial issue.

In the coexistence measurement, some important things were found out. Firstly, the carrier separation up to 2.2 MHz is never sufficient. Then, the carrier separation of 2.4 MHz is on the borderline, it may cause problems. The power control doesn't need to be enough. Finally, the carrier separation of 2.6 MHz is recommended as a reliable minimum, when the problems are excluded. The GSM/EDGE system is more vulnerable in presence of the adjacent wideband UMTS signal, while the UMTS system is more resistant in presence of the adjacent narrowband GSM/EDGE signal. The instruments to reduce these effects of the adjacent channel interference are high quality filters, transmitters with the minimal ACLR and the fast power control.

The further research will be focused on multiple UEs interference investigation, downlink measurements and getting more precise results as the technology will allow.

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